TRILOBIC VIBRANT SYSTEMS

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1. INTRODUCTION

The trilobes are **ex-centric circular supermathematics functions (EC-SMF)** of angular excentricity $\varepsilon = \frac{\pi}{2}$, with notations *cet* θ and *set* θ , for the trilobic ex-centric cosine and, respectively, the trilobic ex-centric sine, with equations:

(1)
$$\begin{cases} cet\theta = cex\left[\theta, S\left(s, \frac{\pi}{2}\right)\right] = cos\{\theta - arcsin\left[s. sin\left(\theta - \frac{\pi}{2}\right)\right]\} = cos[\theta + arcsin[s. cos\theta]] \\ set\theta = sex\left[\theta, S\left(s, \frac{\pi}{2}\right)\right] = sin\{\theta - arcsin\left[s. sin\left(\theta - \frac{\pi}{2}\right)\right]\} = sin[\theta + arcsin[s. cos\theta]] \end{cases}$$

where **S** is a point, called **ex-center**, from the unity-circle plan of $\mathbf{CU}[O(0, 0), \mathbf{R} = 1]$, of polar coordinates $\mathbf{S}(\mathbf{s}, \boldsymbol{\varepsilon})$, where $\mathbf{s} \in [-1,+1]$ is the **numerical linear ex-centricity**, and $\mathbf{e} = \mathbf{R}\mathbf{s}$ is the **real linear ex-centricity**, for any circle of radius **R**, and $\boldsymbol{\varepsilon}$ is the **angular ex-centricity**.

The graphics of trilobic ex-centric supermathematics functions (TE-SMF) are shown in Figure 1.





The trilobic ex-centric supermathematics functions are abbreviated as (TE-SMF).

It follows that, for a numerical linear ex-centricity $\mathbf{s} = 0$, **TE-SMF** degenerates into **central circular** functions (**CC-SMF**) or **circular functions** / ordinary Euler trigonometric functions $\cos \alpha$ and $\sin \alpha$ ($\mathbf{s} = 0 \rightarrow \alpha \equiv \theta$), and for an angular ex-centricity $\boldsymbol{\varepsilon} = 0$ and $\mathbf{s} \neq 0$, it degenerates in **EC-SMF cex** θ and, respectively, sex θ .



The term of **TE-SMF** derives from the fact that, for $\mathbf{s} \in (0, 1)$, the parametric equations, consisting of a combination of **EC-SMF** and **TE-SMF**, express closed plane curves of **3 lobes**, which, for $\mathbf{s} = 0$, degenerates in a perfect circle and for $\mathbf{s} = \pm 1$ in a **rectangular isosceles triangle (TS)** or in an **ex-centric rectangular isosceles triangle (TC)** \blacktriangleleft , a figure in the shape of **inclined Y**, visible in the graphs of **Figures 2**, a \triangleright .

2. DIFFERENTIAL EQUATION OF TRILOBIC VIBRANT SYSTEMS

Let us have the functions x(t), $y(t) : \mathbb{R} \rightarrow [-1,+1]$ and $\theta = \Omega \cdot t$

(1)
$$\begin{cases} x(t) = \operatorname{cet}[\Omega t, \mathbf{S}(s, \varepsilon)] \\ y(t) = \operatorname{set}[\Omega t, \mathbf{S}(s, \varepsilon)] \end{cases}$$

of the same ex-center $S(s, \varepsilon)$, where s is the polar radius and ε – the polar angle, in a unity-circle of radius **R** = 1 \rightarrow CU(O,1).

Their derivatives, for $\theta = \Omega$.t and $\frac{d\theta}{dt} = \Omega = 1$, are: (2) $\begin{cases} \dot{x}(t) = \frac{d}{dt} \operatorname{cet}[\Omega t, \mathbf{S}(s, \varepsilon)] = \frac{d\theta}{dt} \frac{d}{d\theta} \operatorname{cet}[\theta, \mathbf{S}(s, \varepsilon)] = \Omega. \frac{d}{d\theta} \operatorname{cet}[\theta, \mathbf{S}(s, \varepsilon)] = -\Omega. \operatorname{det}\theta. \operatorname{set}\theta \\ \dot{y}(t) = \frac{d}{dt} \operatorname{set}[\Omega t, \mathbf{S}(s, \varepsilon)] = \frac{d\theta}{dt} \frac{d}{dt} \operatorname{set}[\theta, \mathbf{S}(s, \varepsilon)] = \Omega. \frac{d}{d\theta} \operatorname{set}[\theta, \mathbf{S}(s, \varepsilon)] = +\Omega. \operatorname{det}\theta. \operatorname{cet}\theta \\ \text{where } \Omega. \operatorname{det}\theta = \omega \text{ and, explicitly:} \end{cases}$

(3)
$$\begin{cases} \dot{x}(t) = -\Omega \cdot \left(1 - \frac{s.\sin\theta}{\sqrt{1 - s^2\cos\theta^2}}\right) \sin[\theta + \arcsin(s.\cos\theta] = -\omega \cdot set\theta \\ \dot{y}(t) = \Omega \cdot \left(1 + \frac{s.\sin\theta}{\sqrt{1 - s^2\cos^2\theta}}\right) \cos[\theta + \arcsin(s.\sin\theta)] = \omega \cdot cet\theta \end{cases}$$

from where we get the expression TE-SMF trilobic ex-centric derivative of ex-centric variable θ : (4) $det\theta = 1 - \frac{s.\sin\theta}{\sqrt{1-s^2\cos\theta^2}} = \frac{d\alpha(\theta)}{d\theta} = \frac{aet\theta}{d\theta}$, with graphics in Figure 3.





The function **trilobic ex-centric amplitude aet** $\theta = \alpha(\theta)$ is represented by the angle $\alpha(\theta)$ or by the **centric variable** α , to the center O(0, 0), as a function of angle θ to the ex-center $S(s, \frac{\pi}{2})$ or of **ex-centric variable** θ (Fig. 4 \triangleright), and Ω . *det* $\theta = \omega(t)$, so that the second derivative of **TE-SMF (3)** is:

(5)
$$\begin{cases} \ddot{x} = \frac{d}{dt}(-\omega.set\theta) = -3.set\theta - \omega^2.cet\theta \\ \ddot{y} = \frac{d}{dt}(\omega.cet\theta) = 3.cet\theta - \omega^2.set\theta \end{cases}$$

where we denoted by $3 = \frac{d\Omega}{dt}$ the angular acceleration of a moving point on the circle of parametric equations expressed by the relations (1), with variable angular speed (4), as it can be observed in **Figure 5**, following the angular distribution of colors.

The wronskian matrix of trilobic system of vibrations is:

(6)
$$\begin{vmatrix} x(t) & y(t) \\ \dot{x}(t) & \dot{y}(t) \end{vmatrix} = \begin{vmatrix} \operatorname{cet}[\Omega t, S(s, \varepsilon)] & \operatorname{set}[\Omega t, S(s, \varepsilon)] \\ -\Omega. \, det\theta. \, set\theta & +\Omega. \, det\theta. \, cet\theta \end{vmatrix} = \Omega. \, det\theta [\operatorname{cet}^2 \theta. + \operatorname{set}^2 \theta] = \Omega. \, det\theta$$

because $\cot^2 \theta + \sec^2 \theta = 1$, as well as their counterparts $\cot^2 \theta + \sec^2 \theta = 1$, as well as their ancestor / precursor archaics $\cos^2 \alpha + \sin^2 \alpha = 1$.

The graphics of **wronskian** matrix, for $\Omega = 1$, are shown in **Figure 3**, from where it can be inferred that the values are strictly positive for $|\mathbf{s}| < 1$ and, by consequence, there is a **linear differential equation**, of a dynamic technical system, of nonlinear elastic property, admitting these functions as fundamental system of solutions.

The fundamental system of solutions is:

(7) $Z = C_1 \operatorname{cet}\Omega t + C_2 \operatorname{set}\Omega t$,

where $C_1, C_2 \in \mathbb{R}$ are constant and (7) is the general solution of the following differential equation. The equations is:

(8)
$$\begin{vmatrix} z & x & y \\ \dot{z} & \dot{x} & \dot{y} \\ \ddot{z} & \ddot{x} & \ddot{y} \end{vmatrix} = 0$$



(9)
$$\ddot{\mathbf{z}}\begin{vmatrix} x & y \\ \dot{x} & \dot{y} \end{vmatrix} - \dot{\mathbf{z}}\begin{vmatrix} x & y \\ \ddot{x} & \ddot{y} \end{vmatrix} + \mathbf{z}\begin{vmatrix} \dot{x} & \dot{y} \\ \ddot{x} & \ddot{y} \end{vmatrix} = 0$$

(8')
$$\begin{vmatrix} z & cet\theta & set\theta \\ \dot{z} & -\omega.set\theta & \omega.cet\theta \\ \dot{z} & -3.set\theta - \omega^2.cet\theta & 3.cet\theta - \omega^2.set\theta \end{vmatrix} = 0$$

(8')
$$\ddot{z}\Big|_{-\omega.set\theta}^{cet\theta} \frac{set\theta}{\omega.cet\theta}\Big| - \dot{z}\Big|_{-3.set\theta}^{cet\theta} \frac{\omega}{\omega^2.cet\theta} \frac{set\theta}{3.cet\theta - \omega^2.set\theta}\Big| +$$

$$z \begin{vmatrix} -\omega \cdot set\theta & \omega \cdot cet\theta \\ -3 \cdot set\theta - \omega^2 \cdot cet\theta & 3 \cdot cet\theta - \omega^2 \cdot set\theta \end{vmatrix} = 0$$

(10) $\ddot{\mathbf{z}}.\,\omega(\operatorname{cet}^{2}\theta + \operatorname{set}^{2}\theta) - \dot{\mathbf{z}}.\,[3.\,\operatorname{cet}^{2}\theta - \omega^{2}.\,\operatorname{cet}\theta\operatorname{set}\theta + 3.\,\operatorname{set}^{2}\theta + \omega^{2}.\,\operatorname{cet}\theta.\,\operatorname{set}\theta] + \mathbf{z}[-3.\,\omega.\,\operatorname{cet}\theta\operatorname{set}\theta + \omega^{3}.\,\operatorname{set}^{2}\theta + 3.\,\operatorname{\omegaset}\theta.\,\operatorname{cet}\theta + \omega^{3}.\,\operatorname{cet}^{2}\theta] = 0$

(10')
$$\ddot{z}.\omega - \dot{z}.3 + z.\omega^3 = 0$$

or

(10")
$$\ddot{z} - \dot{z} \frac{3}{\omega} + z \omega^2 = 0$$

which is the differential equation of open, unamortized vibrations, of **neuron** mechanical systems, identical equation, **<u>in form</u>**, with the equation of open, unamortized vibrations of **ex-centric** systems, and with the equation of **quadrilobic** ones.

3. INTEGRAL CURVES IN THE PHASE PLANE

The integral curves are the plane curves described by the speed points rotating on the unity-circle of $\mathbf{R} = 1$, or on another circle of radius equally to the maximum amplitude of oscillation $\mathbf{R} = A$, according to their projection position on the axis Ox, i.e. V(x) and are sunt shown in **Figure 6**.

Their parametric equations are:

• for trilobes C
(
$$x = cet\theta$$

(11)
$$\begin{cases} y = -\Omega, det\theta, set\theta \end{cases}$$

• for trilobes S

(12)
$$\begin{cases} x = set\theta \\ y = 0 dot0 sot \end{cases}$$

 $y = \Omega. det\theta. cet\theta$

with graphics in Figure 6, a and, respectively, 6, b.



In the case of open, unamortized vibrations, there are only two forces in the system:

• the force exerted by the elastic element of the system, proportional to the movement x, namely

(13) $F_{el} = \mathbf{k} \cdot \mathbf{x} = \begin{cases} \mathbf{k} \cdot \mathbf{cet} \Omega t \\ \mathbf{k} \cdot \mathbf{set} \Omega t \end{cases}$

where k is an elastic constant of the element and the acceleration force, proportional to the **mass m** of the oscillating system and to the mass acceleration of the system, i.e.



(14)
$$\mathbf{F}_{acc} = \mathbf{m}.\ddot{\mathbf{x}} = \begin{cases} \boldsymbol{m}(-3.set\theta - \omega^2.cet\theta) \\ \boldsymbol{m}(+3.cet\theta - \omega^2.set\theta) \end{cases}$$

4. STATIC ELASTIC PROPERTIES (SEP) OF TRILOBIC OSCILLATING SYSTEMS

Since there are only two forces in the considered system, under condition of dynamic equilibrium, they must be equal and of contrary signs / directions, meaning that

(15) $F_{el} + F_{acc} = 0$, $\rightarrow F_{el} = -F_{acc}$ and, as a result, the static elastic properties (SEP) of trilobic systems are expressed by the parametric equations:

(16)
$$\begin{cases} x = cet\theta \\ y = \ddot{x} = -(-3.set\theta - \omega^2.cet\theta) \end{cases}$$

and, explicitly, for trilobic systems C:

$$(16') \quad \begin{cases} x = \cos[\theta + \arcsin(s.\cos\theta] \\ y = -(-\cos[x + \arcsin[s\cos[x]]]) \left(1 - \frac{s.\sin[x]}{\sqrt{1 - s^2\cos[x]^2}}\right)^2 - \left(-\frac{s\cos[x]}{\sqrt{1 - s^2\cos[x]^2}} + \frac{\cos[x]\sin[x]^2}{(1 - 1s^2\cos[x]^2)^{3/2}}\right) \sin[x + \arcsin[s.\cos[x]]]) \end{cases}$$

with graphics in **Figure 7** \wedge , while for **trilobic systems S**, the parametric equations are:

(17)
$$\begin{cases} x = set\theta \\ y = \ddot{y} = -(3. cet\theta - \omega^2. set\theta) \end{cases}$$

and, explicitly:

$$x = \sin[\theta + \arcsin(s. \cos\theta]$$

$$(17') \begin{cases} y = -(\cos[x + \arcsin[s. \cos[x]]](-\frac{\sin[x]}{\sqrt{1-s^2\cos[x]^2}} + \frac{s^3\cos[x]\sin[x]^2}{(1-s^2\cos[x]^2)^{3/2}}) - \left(1 - \frac{s\sin[x]}{\sqrt{1-s^2\cos[x]^2}}\right)^2 \sin[x + \arcsin[s. \cos[x]]])$$
with graphics in **Figure 7V**.





From graphics in **Figure 7**, it follows that **SEP linear** for $\mathbf{s} = \mathbf{0}$, as it was expected, since we are in this case in the **centric field**, of classical linear systems of vibrations, expressed by circular centric functions $\cos \alpha$ and $\sin \alpha$, but also for $\mathbf{s} = \pm 1$, which is a less expected result, even a surprise, which also appeared with the other systems expressed by **supermathematic functions** mentioned above (**quadrilobes**, expressed by **quadrilobic functions coq** θ and **siq** θ , but alo by **SMF- ex-centric circular**, by functions **cex** θ and **sex** θ).

REFERENCES

1	Şelariu Mircea Eugen	STUDIUL VIBRAȚIILOR LIBERE ALE UNUI SISTEM NELINIAR, CONSERVATIV CU AJUTORUL FUNCȚIILOR CIRCULARE	Com. I Conf. Naţ. Vibr.în C.M. Timişoara, 1978, pag. 95100
2	Şelariu Mircea Eugen	EXCENTRICE FUNCȚIILE SUPERMATEMATICE CIRCULARE EXCENTRICE cexθ și sexθ DE VADIARI Ă EXCENTRICĂ θ –	Com. A VII-a Conf.Naţ. V.C.M., Timişoara, 1993, pag. 275284.
3	Şelariu Mircea Eugen	DE VARIABILA EXCENTRICA U – SOLUȚIILE UNOR SISTEME MECANICE NELINIARE FUNCȚIILE SUPERMATEMATICE CIRCULARE EXCENTRICE Cexα și Sexα DE VARIABILĂ CENTRICĂ α CA SOLUȚII	TEHNO '98. A VIII-a Conferința de Inginerie Managerială și Tehnologică, Timișoara 1998, pag 557572
4	Şelariu Mircea Eugen	ALE UNOR SISTEME OSCILANTE NELINIARE QUADRILOBIC VIBRATION SYSTEMS	The 11th International Conference on Vibration Engineering, Timişoara, Sept. 27-30, 2005 pag. 77 82

5	Şelariu Mircea Eugen	SUPERMATEMATICA. FUNDAMENTE, Second edition, Vol. I and Vol. II	Editura POLITEHNICA, Timișoara, 2012
6	Şelariu Mircea Eugen	SUPERMATEMATICA. FUNDAMENTE,	Editura POLITEHNICA, Timișoara, 2007
7	Şelariu Mircea Eugen	FUNCȚII CIRCULARE EXCENTRICE	Com. I Conferință Națională de Vibrații în Construcția de Mașini, Timișoara, 1978, pag.101108.
8	Şelariu Mircea Eugen	FUNCȚII CIRCULARE EXCENTRICE și EXTENSIA LOR.	Bul. St.şi Tehn. al I.P. "TV" Timişoara, Seria Mecanică, Tomul 25(39), Fasc. 1- 1980, pag. 189196
9	Şelariu Mircea Eugen	RIGIDITATEA DINAMICĂ EXPRIMATĂ CU FUNCȚII SUPERMATEMATICE	Com.VII Conf. Internaţ. De Ing. Manag. Si Tehn., TEHNO '95 Timişoara, 1995 Vol.7 : Mecatronică, Dispoz. Si Rob. Ind., pag. 185194
10	Şelariu Mircea Eugen	DETERMINAREA ORICÂT DE EXACTĂ A RELAȚIEI DE CALCUL A INTEGRALEI ELIPTICE COMPLETE DE SPETA ÎNTÂIA K(k)	Bul. VIII-a Conf. De Vibr. Mec., Timișoara, 1996, Vol III, pag.15 24.
11	Şelariu Mircea Eugen	SMARANDACHE STEPPED FUNCTIONS	"Scienta Magna" Vol. 3, No. 1, 2007, ISSN 1556-6706
12	Şelariu Mircea Eugen	TEHNO ART OF ȘELARIU SUPERMATHEMATICS FUNCTIONS	(ISBN-10):1-59973-037-5 (ISBN-13):974-1-59973-037-0 (EAN): 9781599730370
13	Preda Horea	REPREZENTAREA ASISTATĂ A TRAIECTORILOR ÎN PLANUL FAZELOR A VIBRAȚIILOR NELINIARE	Com. VI-a Conf. Naţ. Vibr. în C.M. Timişoara, 1993
15	Smarandache Florentin	IMMEDIATE CALCULATION OF SOME	http://arxiv.org/abs/0706.4238 Archiv
	Şelariu Mircea Eugen	SUPERMATHEMATICS CIRCULAR EX- CENTRIC FUNCTIONS	viXra.org > Functions and Analysis > viXra:1004.0053
16	Şelariu Mircea Eugen	MIȘCAREA CIRCLARĂ EXCENTRICĂ. PENDULUL SUPERMATEMATIC	www.cartiaz.ro pag. 3
17	Şelariu Mircea Eugen	ELEMENTE NELINIARE LEGATE ÎN Sedie	www.cartiaz.ro pag. 3
18	Şelariu Mircea Eugen	SERIE RIGIDITATEA DINAMICĂ EXPRIMATĂ CU FUNCȚII SUPERMATEMATICE	www.cartiaz.ro pag. 4
19	Şelariu Mircea Eugen	OPTIMIZAREA TRANSPORTULUI VIBRAȚIONAL CU AJUTORUL FUNCȚIILOR SUPERMATEMATICE CIDCUL ABE EXCENTRICE (ESM. CE)	www.cartiaz.ro pag. 4
20	Şelariu Mircea Eugen	O METODA NOUA DE INTEGRARE. INTEGRAREA PRIN DIVIZAREA DIFERENȚIALEI	www.cartiaz.ro pag. 4
21	Şelariu Mircea Eugen	INTEGRALE SI FUNCȚII ELIPTICE EXCENTRICE	www.cartiaz.ro pag. 4
22	Şelariu Mircea Eugen	LOBELE - CURBE MATEMATICE NOI	<u>www.cartiaz.ro</u> pag. 6

ANEXA 1



